# **Multi-Vehicle Velocity Estimation Using IEEE 802.11ad Waveform**

Geonho Han\*, Sucheol Kim, and Junil Choi

School of Electrical Engineering

Korea Advanced Institute of Science and Technology, Daejeon, Korea 34141

ghhan6, loehcusmik, junil@postech.ac.kr



### ABSTRACT

- Use of millimeter wave (mmWave) spectra for wireless communications
  - enable extra radar functionalities
- Dual functional systems for radar and communications
- reduced power consumption & physical space
- jointly optimized especially for vehicular environments
- IEEE 802. I lad waveform
- good correlation property of preamble suitable for target sensing
- Proposed multi-vehicle velocity estimation technique

# **DOPPLER SHIFT ESTIMATION**

**Backscattering coefficient estimation** 

- Approximation at the 0-th frame by the small symbol period  $T_s$  (wide bandwidth)  $\hat{P}-1$  $y[0,k] \approx \sum_{p=0} \sqrt{P_{\mathrm{TX}}} s[k - \hat{\ell}_p^0] h_p + z[0,k]$  $e^{j2\pi\nu_p^0kT_s} \approx 1$ 

- Least square estimation (LSE) concatenating all the echo samples

- form a wide beam to detect multiple target vehicles
- estimate round-trip delays and Doppler shifts
- compensate the phase wrapping in Doppler shifts

#### SYSTEM MODEL

A vehicle-to-vehicle (V2V) multi-target scenario 



- Two-way radar channel model 
  $$\begin{split} \mathbf{H}(t) &= \sum_{p=0}^{P-1} \sqrt{G_p(t)} \beta_p e^{j2\pi t \nu_p(t)} e^{-j2\pi f_c \tau_p(t)} \mathbf{a}_{\mathrm{RX}}^*(\phi_p(t), \theta_p(t)) \mathbf{a}_{\mathrm{TX}}^{\mathrm{H}}(\phi_p(t), \theta_p(t)) \\ P : \text{The number of target vehicles} \qquad \nu_p(t) : \text{Doppler shift} \qquad \phi_p(t) : \text{Azimuth angle} \end{split}$$
- $\mathbf{y}_0 = \sqrt{P_{\mathrm{TX}}} \mathbf{S}_0 \mathbf{h} + \mathbf{z}_0 \qquad \qquad \mathbf{LSE} \qquad \hat{\mathbf{h}} = \frac{(\mathbf{S}_0^{\mathrm{H}} \mathbf{S}_0^{\mathrm{H}})^{-1} \mathbf{S}_0^{\mathrm{H}} \mathbf{y}_0}{\sqrt{P_{\mathrm{TX}}}}$ **Effective radar channel estimation** K : the number of samples in one frame - Approximation for posterior frames using the fact  $k \ll mK$  $y[m_{\rm d},k] \approx \sum_{p=0}^{P-1} \sqrt{P_{\rm TX}} s[k - \hat{\ell}_p^{m_{\rm d}}] h_p e^{j2\pi\nu_p^{m_{\rm d}}((2\hat{\ell}_0^{m_{\rm d}} + K_{\rm pre} - 1)/2 + m_{\rm d}K)T_s} + z[m_{\rm d},k]$  $\longleftarrow \text{ Effective radar channel}$ - Least square estimation (LSE) concatenating all the echo samples **Doppler shift estimation**  $\hat{\nu}_{p}^{m_{\rm d}} = \frac{\angle (h_{m_{\rm d}}[p]/h[p])}{2\pi ((2\hat{\ell}_{0}^{m_{\rm d}} + K_{\rm pre} - 1)/2 + m_{\rm d}K)T_{s}} \quad (p = 0, \cdots, \hat{P} - 1)$ Phase wrapping compensation
- Magnitude difference of Doppler shift estimates  $\hat{c}_p = |\hat{\nu}_p^{m_d}| - |\hat{\nu}_p^{m_i}|$  for  $p = 0, 1, \cdots, \hat{P} - 1$
- For true phases  $c_p = |\nu_p^{m_{\rm d}}| - |\nu_p^{m_{\rm i}}|$  $= |\zeta_p^{m_{\rm d}} D_{m_{\rm d}}| - |\zeta_p^{m_{\rm i}} D_{m_{\rm i}}|$  $= |(2\pi N_p + \zeta_{p,\text{wrap}}^{m_{d}})D_{m_{d}}| - |(2\pi N_p + \zeta_{p,\text{wrap}}^{m_{i}})D_{m_{i}}|$

$$\begin{split} \zeta_p^{m_{\rm d}} &= \angle (\hat{h}_{m_{\rm d}}[p]/\hat{h}[p]) \\ D_{m_{\rm d}} &= \frac{1}{2\pi ((2\hat{\ell}_0^{m_{\rm d}} + K_{\rm pre} - 1)/2 + m_{\rm d}K)T_s} \end{split}$$

 $G_{\mathcal{D}}(t)$ : Large-scale channel gain  $au_p(t)$  : Round-trip delay  $heta_p(t)$  : Elevation angle  $\beta_p$ : Small-scale complex channel gain ~  $\mathcal{CN}(0,1)$ - Wide beam  $N_c$  :The number of combined beams  $\varphi_i$  :Azimuth angle of the *i*-th beam  $\gamma_i$  :Weight coefficient for the *i*-th beam  $\vartheta_c$  : Fixed elevation angle - Radar echo signal model  $y[m,k] = \sum_{m=1}^{n} \sqrt{P_{\text{TX}}} h_p e^{j2\pi \nu_p^m (k+mK)T_s} s[k - \ell_p^m] + z[m,k]$  $h_p$ : Backscattering coefficient  $(h_p \approx \sqrt{G_p} \beta_p \mathbf{f}_{\mathrm{RX}}^{\mathrm{H}} \mathbf{a}_{\mathrm{RX}}^*(\phi_p, \theta_p) \mathbf{a}_{\mathrm{TX}}^{\mathrm{H}}(\phi_p, \theta_p) \mathbf{f}_{\mathrm{TX}})$  $- \begin{array}{ccc} m = 0, 1, \cdots, M - 1 & M : \text{the number of frames in one coherent processing interval (CPI)} \\ k = \ell_0^m, \ell_0^m + 1, \cdots, K_{\text{pre}} - 1 + \ell_0^m & K_{\text{pre}} : \text{the number preamble samples} \end{array}$ 

## **DELAY ESTIMATION**

- **Golay complementary sequences**
- Used for the preamble of IEEE 802. I lad waveform
- Correlation property

$$\mathbf{a}_{N} = [a_{0}, a_{1}, ..., a_{N-1}]^{\mathrm{T}}, \mathbf{b}_{N} = [b_{0}, b_{1}, ..., b_{N-1}]^{\mathrm{T}}$$
$$R_{\mathbf{a}_{N}}[k] + R_{\mathbf{b}_{N}}[k] = 2N\delta[k], \text{ where } R_{\mathbf{c}}[k] = \sum_{k=1}^{N-k-1} c[q]c[q+k],$$

#### **Vehicular velocity**

- Using the definition of Doppler shift & small angle approximation

## **SIMULATION RESULTS**



- Simulation set-up
- 3dB azimuth beamwidth: 0.4084 rad
- TX anteanns: 8x2 UPA
- RX antennas: 8x2 UPA
- Comparison scheme [1] - use delay-Doppler map estimation



• The proposed technique outperforms the scheme in [1] for all CPI values even with lower TX power than [1].

## High velocity estimation accuracy within a short CPI

#### REFERENCE

[1] P. Kumari, J. Choi, N. Gonz'alez-Prelcic, and R.W. Heath, "IEEE 802.11 ad-Based Radar: An Approach to Joint Vehicular Communication-Radar System," IEEE Trans. Veh. Technol., vol. 67, no. 4, pp. 3012–3027, 2017.

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