

PERCEPTUALLY MOTIVATED ANALYSIS OF NUMERICALLY SIMULATED HEAD-RELATED TRANSFER FUNCTIONS GENERATED BY VARIOUS 3D SURFACE SCANNING SYSTEMS

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Abstract

Numerical simulations offer a feasible alternative to the direct acoustic measurement of individual head-related transfer functions (HRTFs). For the acquisition of high quality 3D surface scans, as required for these simulations, several approaches exist. In this paper, we systematically analyze the variations between different approaches and evaluate the influence of the accuracy of 3D scans on the resulting simulated HRTFs. To assess this effect, HRTFs were numerically simulated based on 3D scans of the head and pinna of the FABIAN dummy head generated with 6 different methods. These HRTFs were analyzed in terms of interaural time difference, interaural level difference, energetic error in auditory filters and by their modeled localization performance. From the results, it is found that a geometric precision of about 1 mm is needed to maintain accurate localization cues, while a precision of about 4 mm is sufficient to maintain the overall spectral shape.

Motivation

- > In recent years, several approaches have been proposed with a focus on increasing the accuracy of the simulated HRTF by acquiring high quality 3D scans of head and pinna. Different techniques for the acquisition of 3D surface scans exist such as MRI scanners, structured light scanners, laser scanners, infrared scanners, stationary scanners, hand held scanners, or by using mobile camera pictures [1].
- > Each of them provides a different resolution and its accuracy directly affects the quality of the numerically simulated HRTFs which are subject to research.
- > Here, we systematically analyze the accuracy of 3D surface scans obtained by different approaches and study their influence on the resulting HRTFs by means of interaural time difference (ITD), interaural level difference (ILD), energetic error in equivalent rectangular bandwidth (ERB) auditory filters, and their simulated localization performance.
- > To isolate the influence of the scanning method on the HRTF, the different scanning methods were evaluated against a high resolution structured light scan (ground truth) which showed a very good agreement to its acoustically measured correspondent in an earlier study [2].

Acquisition of Meshes using different scanning systems

We acquired 3D surface scans of the head and pinna of the FABIAN dummy head by using 6 different methods (cf. Fig.1).

- a) GOM ATOS-I (GOM-Ref): Stationary, structured light scanner (0.01 mm point resolution).
- **b)** Artec Spider (SPY): Hand-held structured light scanner, scanning at a working distance of 0.2 m to 0.3 m (0.05 mm point resolution).
- c) Canfield Vectra M3 (CAN): Stationary, stereo photogrammetry technology scanning at a working distance 1 m (1 mm point resolution).
- d) Microsoft Kinect (KIN): Low cost IR scanner with a working distance between 0.5 m to 1 meter.
- e) Autodesk 123D catch (123D): Mobile application which allows the user to get a 3D model from at least 5 to 6 overlapping photos.
- f) The Python Photogrammetry Toolbox (PPT): An open source tool which has a pipeline to construct a 3D model from a set of photos.
- (- iPhone 6 mobile was used to take photos for 123D and PPT method)

was used [5].



Fig 2: Geometric difference of (i) SPY, (ii) CAN, (iii) KIN, (iv) 123D and (v) PPT with respect to GOM-Ref (in mm)



Fig 1: FABIAN 3D Surface Scans using (a) GOM ATOS-I Scanner (GOM-Ref), (b) Artec Space Spider Scanner (SPY), (c) Canfield Vectra M3 scanner (CAN), (d) Kinect scanner (KIN), (e) Autodesk 123D (123D), and (f) PPT (PPT).

Alignment , Re-meshing & HRTF Simulations

1) In the first step, interaural axis and interaural center of the **GOM-Ref** mesh were aligned to the origin of coordinates. 2) Then, the remaining FABIAN surface scans were then aligned with respect to GOM-Ref using the iterative closest point (ICP) algorithm from the surface manipulation and transformation toolkit (SUMATRA) [3].

3) A priori mesh grading algorithm (resulting in non-uniform meshing) was deployed according to Ziegelwanger et al. which result in increases in size of the mesh element with respect to the distance from the ear [4].

4) Two different models were generated for each scanning method: One for the left pinna (with small mesh elements at the left ear, and large elements at the right), and one for the right pinna.

5) The target lengths used were 1 mm to 10 mm, which resulted in around 20,000 elements per mesh.

6) For numerical HRTF simulation, the Mesh2HRTF implementation of the 3-dimensional Burton-Miller collocation BEM

Difference in terms of Geometrics and Localization performance





Scans	$X_1(\mu,\sigma)$	$X_2(\mu,\sigma)$	X 3 (тах)	X 4 (max)	X ₅ (max)	Х ₆ (тах)
SPY	0.14 (0.24)	0.17 (0.29)	0.50	0.75	0.75	0.75
CAN	0.66 (0.80)	0.66 (0.54)	0.66	0.90	0.90	0.80
KIN	1.53 (0.28)	1.50 (1.08)	1.50	2.50	1.25	1.25
123D	1.98 (1.42)	2.10 (1.41)	5.00	3.75	2.50	3.75
PPT	1.77 (1.72)	1.68 (1.56)	5.00	5.00	3.75	5.00

Table 1: Geometric difference in mm ($\mu \rightarrow$ mean, $\sigma \rightarrow$ standard deviation, $max \rightarrow$ maximum difference). $X_1 \rightarrow$ head, $X_2 \rightarrow$ head without pinna, $X_3 \rightarrow$ Concha, $X_4 \rightarrow$ Antihelical fold, $X_5 \rightarrow$ Antihelix and $X_6 \rightarrow$ Fossa.

Measures/ Scans	SPY	CAN	KIN	123D	PPT
PE	< 0.7°	< 0.7°	6°	11°	12°
QE	< 0.4	< 0.4	4	6	6
S _d	< 0.5	< 0.5	< 1	1-2	1-2

Table 2: **PE**, **QE** \rightarrow increase in polar error (in degree), quadrant error (in %) and $S_d \rightarrow$ Average spectral difference (in dB)





[5]. H. Ziegelwanger, W. Kreuzer and P. Majdak, "Mesh2HRTF: An open-source software package for the numerical calculation of headrelated transfer functions," 22nd International Congress on Sound and Vibration, Florence, Italy, 2015.