- A large number of transmitters are often available.
- receivers.
- It is necessary to design the receivers wisely to control the complexity cost.

Received Signal Model

• The received target-present signal at the *n*-th receiver:

$$r_n(t) = \sum_{m=1}^{M} \frac{\beta_{mn} \sqrt{E_m}}{R_{t,m} R_{r,n}} s_m(t - \tau_{mn}) + w_n(t),$$

- β_{mn} , τ_{mn} -reflection coefficient and time delay for mn-th path. β_{mn} is correlated complex Gaussian;
- $R_{t,m}$, $R_{r,n}$ distance between the m-th transmitter/n-th receiver and target;
- E_m , $s_m(t)$ transmitted energy, known waveform from m-th transmitter. Assume direct path antenna gives accurate $s_m(t)$;
- $w_n(t)$ zero-mean complex Gaussian temporally white clutter-plus-noise such that $\mathbb{E}\{w_i(t)w_i^*(u)\} = N_{ij}\delta(t-u)$.

Detection Problem

• Hypothesis Testing Problem

$$\mathcal{H}_0 : r_n(t) = w_n(t)$$

 $\mathcal{H}_1 : r_n(t) = \sum_{m=1}^M \xi_{mn} s_m(t - \tau_{mn}) + w_n(t).$

 $-\xi_{mn} = \beta_{mn} \sqrt{E_m} / (R_{t,m} R_{r,n})$ • Optimal Test Statistic (TS)

$$\mathcal{T} = \boldsymbol{x}^{H} (\boldsymbol{\Sigma}_{0}^{-1} - \boldsymbol{\Sigma}_{1}^{-1})$$

$$m{x} = [m{x}_1^T, ..., m{x}_N^T]^T$$

where

$$\boldsymbol{x}_n = [x_{11n}, \dots, x_{MNn}]^T$$

in which

$$x_{mn'n} = \int_{\mathcal{T}_m} s_m^*(t - \tau_{mn'}) r_n(t) dt$$

is the output of the mn'-th matched filter (MF) at receiver n. TS depends on MF outputs vector. We use them in receiver design problem.

- The terms

$$egin{aligned} oldsymbol{\Sigma}_0 &= oldsymbol{N} \otimes oldsymbol{\Xi} \ oldsymbol{\Sigma}_1 &= oldsymbol{N} \otimes oldsymbol{\Xi} + oldsymbol{\Psi} oldsymbol{\Lambda} oldsymbol{\Psi}^H \end{aligned}$$

are the covariance matrices of $m{x}$ under \mathcal{H}_0 and \mathcal{H}_1 respectively; - $\Lambda = \mathbb{E} \{ \boldsymbol{\xi} \boldsymbol{\xi}^H \}$ is the covariance matrix of $\boldsymbol{\xi} = [\xi_{11}, ..., \xi_{MN}]^T$;

- Ξ is an $MN \times MN$ matrix and

 $\boldsymbol{\Xi}_{(n_1-1)M+m_1,(n_2-1)M+m_2} = \int_{\mathcal{T}_{m_1}} s^*_{m_1} (t - \tau_{m_1n_1}) s_{m_2} (t - \tau_{m_2n_2}) dt;$

- $\Psi = \mathsf{Diag}\{\Psi_1, ..., \Psi_N\}$, where Ψ_n is an $MN \times M$ matrix whose *i*-th column is the ((n-1)M+i)-th column of Ξ .

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Background

• Processing additional transmitters requires additional hardware or software complexity at the

Receiver Design Method

- Define: $\boldsymbol{a} \triangleq [\boldsymbol{a}_1^T, \boldsymbol{a}_2^T, ..., \boldsymbol{a}_N^T]^T$, where $\boldsymbol{a}_n = [\boldsymbol{a}_{11n}, ..., \boldsymbol{a}_{MNn}]^T$ and $a_{mn'n} \in \{1, 0\}$ indicating whether or not the (m, n')-th MF is selected at the *n*-th receiver and a selection vector $J_n(a_n)$, where $\boldsymbol{J}_n(\boldsymbol{a}_n)$ has one unit element per row. The other elements are zeroes.
- Example:

$$\boldsymbol{a}_{1} = \begin{bmatrix} 1 \ 0 \ 1 \ 0 \end{bmatrix}^{T}$$
$$\boldsymbol{J}_{1}(\boldsymbol{a}_{1}) = \begin{bmatrix} 1 \ 0 \ 0 \ 0 \end{bmatrix}^{T}$$
$$\boldsymbol{J}_{1}(\boldsymbol{a}_{1}) \begin{bmatrix} x_{111} \\ x_{121} \\ x_{211} \\ x_{221} \end{bmatrix} = \begin{bmatrix} x_{111} \\ x_{211} \\ x_{211} \end{bmatrix}$$

Put "a" on diagonal and removal all 0 rows.

- The MF output vector at receiver n is reduced from \boldsymbol{x}_n to $\boldsymbol{J}_n(\boldsymbol{x}_n)$.
- The TS becomes

$$egin{aligned} T_s &= \left(oldsymbol{J}(oldsymbol{a})oldsymbol{x}^H \left(\left(oldsymbol{J}(oldsymbol{a})oldsymbol{\Sigma}_0oldsymbol{J}^T(oldsymbol{a})
ight)^{-1} \ &- \left(oldsymbol{J}(oldsymbol{a})oldsymbol{\Sigma}_1oldsymbol{J}^T(oldsymbol{a})
ight)^{-1}
ight)oldsymbol{J}(oldsymbol{a})oldsymbol{x} \end{aligned}$$

• The receiver design can be described in the following problem: $\max_{\boldsymbol{\zeta}} \ \boldsymbol{a} \in \{0,1\}^{MN^2}$ $Pr(T_s > \gamma(P_{FA}; \boldsymbol{a}), \mathcal{H}_1)$ \mathbf{P}_1

s.t.
$$1 \le \|\boldsymbol{a}_n\|_0 \le A_n, n = 1, 2, ..., N$$

Transmitter selection

• Special Case

- Spatially white reflection coefficients and clutter-plus-noise $\mathbf{\Lambda} = \mathsf{Diag}\{\mathbf{\Lambda}_1, ..., \mathbf{\Lambda}_N\}$, where $\mathbf{\Lambda}_n = \mathsf{diag} \ \{\sigma_{1n}^2 E_1/(R_{t,1}R_{r,n})^2, \}$ $..., \sigma_{Mn}^2 E_M/(R_{t,M}R_{r,n})^2\}$ and $N = N_0 I_N$. - Orthogonal waveforms

$$\int_{\mathcal{T}_m} s_m^*(t-\tau) s_{m'}(t) dt \approx 0 \quad \text{for } m \neq m'$$

• Test Statistic

- The TS becomes

$$T_s = \sum_{n=1}^{N} \sum_{m=1}^{M} \frac{E_m \sigma_{mn}^2}{N_0 (E_m \sigma_{mn}^2 + N_0 (R_{t,m} R_{r,n})^2)} |x_{mn}|^2$$

- Only need MN MFs. Redefine an MN imes 1 selection vector $m{a} = [m{a}_1^T,...,m{a}_N^T]^T$, where $\boldsymbol{a}_n = [a_{1n}, ..., a_{Mn}]^T$. - The TS after selection becomes

$$T_s = \sum_{n=1}^{N} \sum_{m=1}^{M} \frac{E_m a_{mn} \sigma_{mn}^2}{N_0 (E_m \sigma_{mn}^2 + N_0 (R_{t,m} R_{r,n})^2)} |x_{mn}|^2$$

MIMO Radar Target Detection Using Low-Complexity Receiver

MSCNR-based Selection

• **Define** the SCNR of the (m,n)-th path as

$$\eta_{mn} = \frac{E_m \sigma_{mn}^2}{N_0 (R_{t,m} R_{r,n})^2}.$$

The TS can be rewritten as

$$T_s = \sum_{n=1}^N \sum_{m=1}^M \zeta_{mn},$$

where $\zeta_{mn} = rac{
ho_{mn}}{N_0(
ho_{mn}+1)|x_{mn}|^2}$ and $ho_{mn} = \eta_{mn}a_{mn}$.

Let $\boldsymbol{\eta} = [\eta_{11}, ..., \eta_{MN}]$, $\boldsymbol{\rho} = [\rho_{11}, ..., \rho_{MN}]^T$.

Lemma: Denote by $\rho_{(1)}, \rho_{(2)}..., \rho_{(K)}$ the decreasing sequence of nonnegative $\rho_{11}, \rho_{21}, \dots, \rho_{MN}$ and define $\rho_{(K)} = [\rho_{(1)}, \rho_{(2)}]$ $[\dots, \rho_{(K)}]^T$, where K = MN. Let α and β be two feasible solutions

for \mathbf{P}_1 , and correspondingly $\rho_{\alpha} = \alpha \odot \eta$ and $\rho_{\beta} = \beta \odot \eta$. If $\boldsymbol{\rho}_{\boldsymbol{\alpha}(K)} \succeq \boldsymbol{\rho}_{\boldsymbol{\beta}(K)}$, then $P_D(\boldsymbol{\rho}_{\boldsymbol{\alpha}}) \geqslant P_D(\boldsymbol{\rho}_{\boldsymbol{\beta}})$.

Theorem: If the corresponding SCNRs of the selected transmitters at receiver n are the largest A_n values in $\{\eta_{1n}, ..., \eta_{Mn}\}$, we can obtain the optimal solution of \mathbf{P}_1 .

Numerical Examples

• Parameter Set up:

- The PSD of noise $N_i i = 1, i = 1, ..., N$, the transmitted energy $E_m = 10^{13}$, the variance of the mn-th path reflection coefficient $\sigma_{mn}^2 = 1$ for all m, n. - Target located at (0,0) km.

- The transmitted waveform

$$e_m(t) = \frac{1}{\sqrt{T}} \exp(j2\pi f_m t), 0 < t < T$$

where T = 1ms for all m and f_m is the transmitted frequency of m-th transmitter. Define $f = [f_1, ..., f_M]$ the transmitted frequency vector. • Example 1: Special case

- Transmitters: $(x_{t,1}, y_{t,1}) = (0,1) \ km$, $(x_{t,2}, y_{t,2}) = (0, 2) \ km$, and $(x_{t,3}, y_{t,3})$ =(0, 3) *km*;
- Receivers: $(x_{r,1}, y_{r,2}) = (-1, 0) km$ and $(x_{r,2}, y_{r,2}) = (1, 0) km$;
- Frequency vector $\boldsymbol{f} = [\frac{10}{T}, \frac{20}{T}, \frac{30}{T}]$ and $P_{FA} = 10^{-2}$.

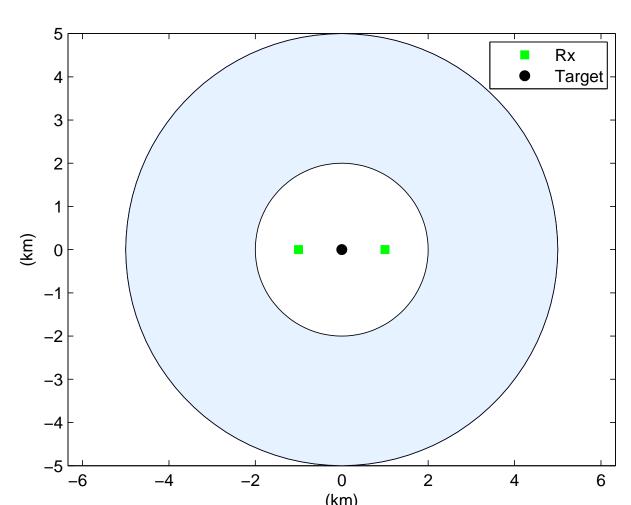
 Table 1: Detection probability of different selections

Selection Combination	SCNR (dB)	P_D
$\{<1,1>,<1,2>\}$	$\{10, 10\}$	0.8798
$\{<1,1>,<2,2>\}$	{10,3.98}	0.7286
$\{<1,1>,<3,2>\}$	$\{10, 0.46\}$	0.6868
$\{<2,1>,<1,2>\}$	$\{3.98, 10\}$	0.7422
$\{<2,1>,<2,2>\}$	{3.98,3.98}	0.4354
$\{<2,1>,<3,2>\}$	{3.98,0.46}	0.3196
$\{<3,1>,<1,2>\}$	$\{0.46, 10\}$	0.6785
$\{<3,1>,<2,2>\}$	{0.46,3.98}	0.3117
$\{<3,1>,<3,2>\}$	{0.46,0.46}	0.1880

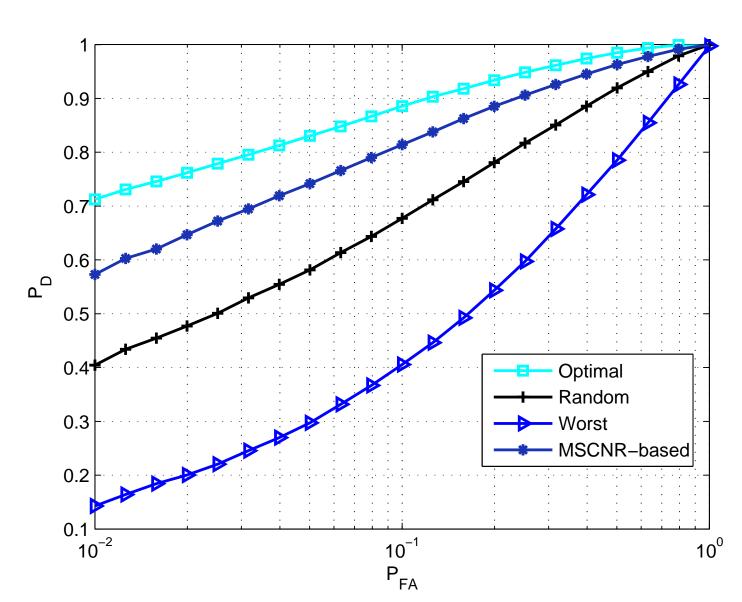
- < m, n > means the *m*-th transmitter being selected at the *n*-th receiver. • Example 2: General case
- Frequency vector $f = [\frac{10}{T}, \frac{20}{T}, \frac{30}{T}]$, $P_{FA} = 10^{-2}$;
- Correlation of clutter-plus-noise $N_{ij}=0.1$, $i, j = 1, 2, i \neq j$;

- Correlation of reflection coefficients $\mathbb{E}\{\beta_{m_1n_1}\beta_{m_2n_2}^*\}=0.1, m_1, m_2=1, ...M,$ $n_1, n_2 = 1, ..., N$, $m_1 \neq m_2$ or $n_1 \neq n_2$;

- 8 transmitters in the wathet area (random placement).

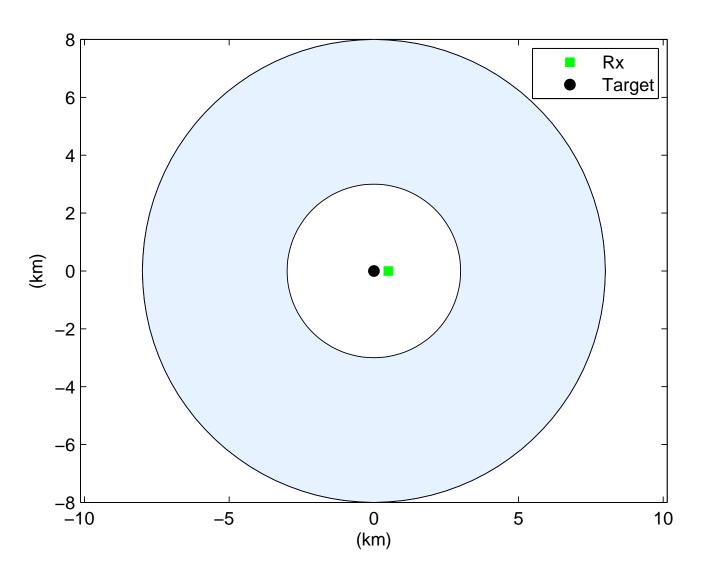


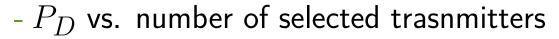
- Different selections

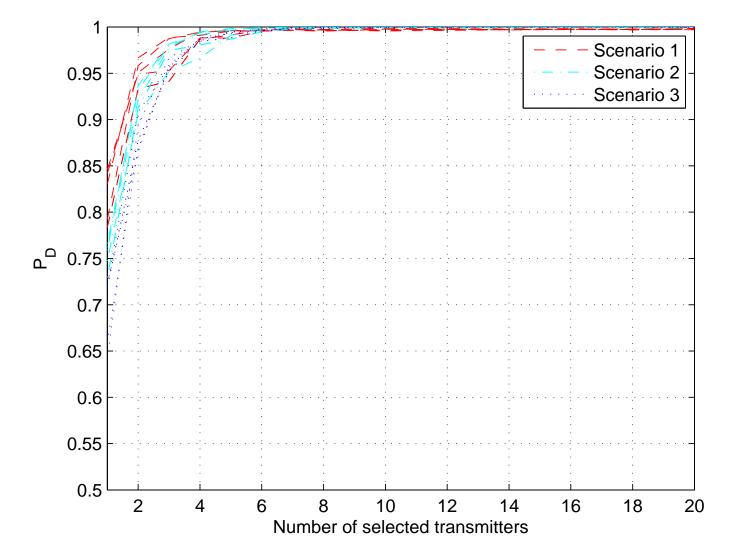


• Example 3: Large number of transmitters

- Frequency vector f is $[\frac{3}{50T}, \frac{6}{50T}, ..., \frac{3}{T}]$ (scenario 1), $[\frac{6}{50T}, \frac{12}{50T}, ..., \frac{6}{T}]$ (scenario 2) and $\left[\frac{9}{50T}, \frac{18}{50T}, ..., \frac{9}{T}\right]$ (scenario 3).
- False alarm probability is 10^{-2} .
- 50 transmitters in the wathet area (random placement).







Conclusion

- Studied low-complexity receiver design for MIMO radar by selecting a limited number of MFs at each receiver due to cost considerations
- For the case of uncorrelated clutter-plus-noise, uncorrelated reflection coefficients, and orthogonal waveforms, at each receiver, maximum P_D can be achieved if we select the transmitters corresponding to the largest SCNRs.
- Selecting a few transmitters can lead to detection performance very close to using all transmitters.

Acknowledgements

The work of Y. Li and Q. He was supported by the National Nature Science Foundation of China under Grants No. 61571091 and 61371184, and Huo Yingdong Education Foundation under Grant No. 161097. The work of R. S. Blum was supported by the National Science Foundation under Grant No. ECCS-1405579.