## Passive Intelligent Surface Assisted MIMO Powered Sustainable IoT

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#### Introduction

- Passive intelligent surface (PIS):
  - a) Remotely programmed via a software controller
  - b) Can alter the electromagnetic behavior of the wireless channel
  - c) Reflecting a phase-shifted version of the incoming signal
  - d) Without requiring any active radio resource for retransmission
- Major bottlenecks include:
  - a) Unawareness about the ungoverned fading channel
  - b) Ultralow power computational capability
- New constant-envelope passive energy beamforming (EB) designs to gain <u>system engineering insights</u>
- Focus: Designing efficient PIS-assisted wireless energy transfer (PET) protocol

#### Literature Review

- Supporting timely energy sustainability demands of wireless devices in Internet-of-things (IoT) [1]
- Some of its implementation designs include:
  - a) Lightweight elements attached to walls or ceilings [2]
  - b) Electronically-controlled resonant frequency-based varactor diodes [3]
  - c) Liquid crystal meta-surfaces fabricated via lithography or nano printing [4]
- Optimal transmit power allocation and phase shifters (PS) design for maximizing sum-rate [5]
- Statistical CSI based study on the effect of PS design on the ergodic spectral efficiency [6]

[1] C. Huang, A. Zappone, M. Debbah, and C. Yuen, "Achievable rate maximization by passive intelligent mirrors," in Proc. IEEE ICASSP, Calgary, Canada, Apr. 2018, pp. 3714–3718.

<sup>[2]</sup> L. Subrt and P. Pechac, "Intelligent walls as autonomous parts of smart indoor environments," IET Commun., vol. 6, no. 8, pp. 1004–1010, May 2012.

 <sup>[3]</sup> S. V. Hum and J. Perruisseau-Carrier, "Reconfigurable reflectarrays and array lenses for dynamic antenna beam control: A review," IEEE Trans. Ant. Prop., vol. 62, no. 1, pp. 183–198, Jan. 2014.
 [4] S. Foo, "Liquid-crystal reconfigurable metasurface reflectors," in Proc. IEEE Int. Symp. on Ant. Prop. (ISAP), San Diego, USA, July 2017, pp. 2069–2070.

<sup>[5]</sup> C. Huang, A. Zappone, M. Debbah, and C. Yuen, "Achievable rate maximization by passive intelligent mirrors," in Proc. IEEE ICASSP, Calgary, Canada, Apr. 2018, pp. 3714–3718.

<sup>[6]</sup> Y. Han, W. Tang, S. Jin, C. Wen, and X. Ma, "Large intelligent surface-assisted wireless communication exploiting statistical csi," IEEE Trans. Veh. Tech., vol. 68, no. 8, pp. 8238–8242, Aug. 2019.

## Multiuser Designs and Research Gap

- SDR and alternating optimization techniques to obtain passive EB designs for PIS-assisted multiuser MISO [7]
- Likewise, two alternating optimization-based efficient energy efficiency maximization algorithms [8]
- Joint active and passive beamforming using random matrix theory tools for max-min goal [9]
- Concerns with existing designs:
  - a) Low-complexity constraints of PIS were ignored
  - b) Perfect CSI availability was assumed
- Compressive sensing-based channel construct approach to obtain the full CSI [10]
- Least-squares (LS) based channel estimation (CE) protocol for single-user setting [11].
- Research Gap: Multiuser CE protocol involving low-complexity EB designs for maximizing sum power during PET

[7] Q. Wu and R. Zhang, "Intelligent reflecting surface enhanced wireless network via joint active and passive beamforming," IEEE Trans. Wireless Commun., vol. 18, no. 11, pp. 5394-5409, Nov. 2019.
 [8] C. Huang, A. Zappone, G. C. Alexandropoulos, M. Debbah, and C. Yuen, "Reconfigurable intelligent surfaces for energy efficiency in wireless communication," IEEE Trans. Wireless Commun., vol. 18, no. 8, pp. 4157–4170, Aug. 2019.

[9] Q.-U.-A. Nadeem, A. Kammoun, A. Chaaban, M. Debbah, and M.-S. Alouin, "Asymptotic analysis of large intelligent surface assisted MIMO communication," arXiv:1903.0812, Apr. 2019.
 [10] C. Liaskos, A. Tsioliaridou, A. Pitilakis, G. Pirialakos, O. Tsilipakos, A. Tasolamprou, N. Kantartzis, S. Ioannidis, M. Kafesaki, A. Pitsillides, and I. Akyildiz, "Joint compressed sensing and manipulation of wireless emissions with intelligent surfaces," in Proc. IEEE DCOSS, Santorini Island, Greece, May 2019, pp. 318–325.

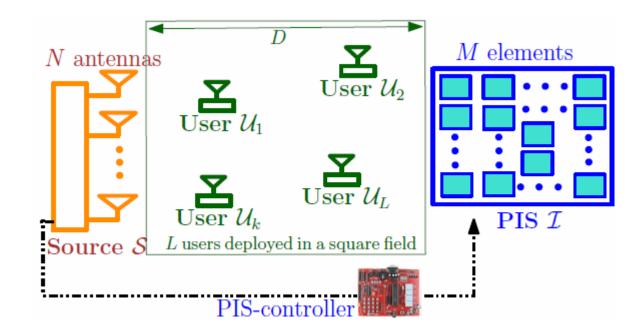
[11] D. Mishra and H. Johansson, "Channel estimation and low-complexity beamforming design for passive intelligent surface assisted MISO wireless energy transfer," in Proc. IEEE ICASSP, Brighton, UK, May 2019, pp. 4659–4663.

#### **Motivation and Contributions**

- Existing passive EB designs are based on computationally-inefficient numerical methods like SDR
- Novel analytical expressions for the jointly-optimal active and passive EB designs are needed
- Practical limitations like unavailability of strong prior for CE
- Overcoming PIS-bottlenecks by to enable sustainable IoT developing closed-form green PS designs
- The key contribution of this work is three-fold:
- a) Novel optimization framework and LS-based CE protocol for the underlying effective cascaded channels to maximize the sum power
- b) Closed-form expressions for optimal active precoder for power beacon (PB) and passive constant-envelope precoding-based PS design
- c) Numerical investigation is carried out to validate the key analytical claims and demonstrate the performance gains over the benchmark

#### System Description

- Multiuser MISO wireless system with:
  - a) L single-antenna IoT users U randomly deployed inside a square-field of length D meters (m)
    b) an N-antenna PB or energy source S
    c) an M-element PIS I installed on the opposite wall
- Flat quasi-static Rician block fading is considered
- PIS has M dynamically reconfigurable low-resolution PS  $\Theta \triangleq \operatorname{diag} \left\{ \alpha_1 e^{j\theta_1} \alpha_2 e^{j\theta_2} \dots \alpha_M e^{j\theta_M} \right\}, \text{ with } j = \sqrt{-1}$
- **PIS-controller** is connected and programmed by PB having all computational resources
- The composite channel involves the concatenation of Sto-I channel, PS matrix at I, and I-to-U channel



#### Channel-Reciprocity Based Downlink MISO PET

- Assuming channel-reciprocity, the downlink (DL) channel coefficients for all links are obtained by estimating them from the uplink (UL) pilot transmission from the IoT users
- Coherence interval is divided into two subphases: UL CE and DL PET
- The combined signal received at IoT users during PET subphase is:

$$\mathbf{y}_{\mathcal{U}} = \left(\mathbf{H}_{\mathcal{S}\mathcal{U}}^{\mathrm{T}} + \mathbf{H}_{\mathcal{I}\mathcal{U}}^{\mathrm{T}} \Theta \mathbf{H}_{\mathcal{S}\mathcal{I}}^{\mathrm{T}}\right) \mathbf{f}_{\mathrm{A}} x_{e} + \mathbf{w}_{\mathcal{U}} = \mathbf{G} \mathbf{f}_{\mathrm{A}} x_{e} + \mathbf{w}_{\mathcal{U}} \qquad \text{where } \mathbf{G} \triangleq \mathbf{H}_{\mathcal{S}\mathcal{U}}^{\mathrm{T}} + \mathbf{H}_{\mathcal{I}\mathcal{U}}^{\mathrm{T}} \operatorname{diag}\left\{\mathbf{f}_{\mathrm{P}}\right\} \mathbf{H}_{\mathcal{S}\mathcal{I}}^{\mathrm{T}}$$

• Sum signal power as received among the L EH users can be approximated to:

$$\|\mathbf{y}_{\mathcal{U}}\|^2 \approx \mathcal{P}_{\mathcal{U}} \triangleq p_e \left\| \left( \mathbf{H}_{\mathcal{S}\mathcal{U}}^{\mathrm{T}} + \mathbf{H}_{\mathcal{I}\mathcal{U}}^{\mathrm{T}} \operatorname{diag} \left\{ \mathbf{f}_{\mathrm{P}} \right\} \mathbf{H}_{\mathcal{S}\mathcal{I}}^{\mathrm{T}} \right) \mathbf{f}_{\mathrm{A}} \right\|^2$$

#### **On-Off PIS Design Based Channel Estimation**

- Binary-reflection (on or off) based CE protocol for multiuser PET is proposed
- PB estimates the CSI for all the links on an element-by-element basis at PIS over **M + 1 subphases**
- Constants  $\epsilon_0$  and  $\epsilon_1$  model realistic implementation errors in ON and OFF modes
- The entries of the combined PS matrix during the CE phase are:

$$[\Phi]_{i,m} \triangleq \begin{cases} 1 - \epsilon_1, & i = m + 1, \\ 0 + \epsilon_0, & \text{otherwise,} \end{cases} \quad \forall i \in \mathcal{M}, \ m \in \mathcal{M}_+, \quad \text{where } \mathcal{M} \triangleq \{1, 2, \dots, M\} \text{ and } \mathcal{M}_+ \triangleq \mathcal{M} \cup \{M + 1\} \end{cases}$$

• The combined received signal matrix at S during CE can be written as:

$$\begin{split} \mathbf{Y}_{\mathcal{S}} &= \Big( \left( \operatorname{vec} \left\{ \mathbf{H}_{\mathcal{S}\mathcal{U}} \, \mathbf{X}_{p} \right\} \otimes \mathbf{1}_{1 \times (M+1)} \right) + \Big( (\mathbf{H}_{\mathcal{I}\mathcal{U}} \, \mathbf{X}_{p})^{\mathrm{T}} \otimes \mathbf{H}_{\mathcal{S}\mathcal{I}} \Big) \Big[ \operatorname{diag} \left\{ \left[ \boldsymbol{\Phi}^{\mathrm{T}} \right]_{1} \right\} \quad \boldsymbol{\mathcal{D}}_{\Phi} \Big] \Big) + \mathbf{W}_{\mathcal{S}} \\ \text{where} \quad \boldsymbol{\mathcal{D}}_{\Phi} &\triangleq \Big[ \operatorname{diag} \left\{ \left[ \boldsymbol{\Phi}^{\mathrm{T}} \right]_{2} \right\} \operatorname{diag} \left\{ \left[ \boldsymbol{\Phi}^{\mathrm{T}} \right]_{3} \right\} \cdots \operatorname{diag} \left\{ \left[ \boldsymbol{\Phi}^{\mathrm{T}} \right]_{M+1} \right\} \Big]^{\mathrm{T}} \end{split}$$

#### **Expressions for LS Estimates**

• The vectorized form for the LS estimate of S-to-U channel matrix as obtained using the pseudoinverse of the pilot matrix can be written as:

 $\operatorname{vec}\left\{\widehat{\mathbf{H}}_{\mathcal{S}\mathcal{U}}\right\} = \left(\left(\mathbf{X}_{\mathrm{p}}^{\dagger}\right)^{\mathrm{T}} \otimes \mathbf{I}_{N}\right) \left[\mathbf{Y}_{\mathcal{S}}^{\mathrm{T}}\right]_{1} = \operatorname{vec}\left\{\mathbf{H}_{\mathcal{S}\mathcal{U}}\right\} + \epsilon_{0}\operatorname{vec}\left\{\mathbf{H}_{\mathcal{S}\mathcal{I}}\mathbf{1}_{M \times M}\mathbf{H}_{\mathcal{I}\mathcal{U}}\right\} + \frac{\mathbf{X}_{\mathrm{p}}^{*} \otimes \mathbf{I}_{N}}{p_{c}\tau_{c}}\left[\mathbf{W}_{\mathcal{S}}^{\mathrm{T}}\right]_{1}$ 

• Finally, using the LS estimate  $\hat{\mathbf{H}}_{SU}$  of  $\mathbf{H}_{SU}$  defined, the LS estimate for the cascaded channel matrix  $\mathcal{G} \triangleq (\mathbf{H}_{IU}^{T} \otimes \mathbf{H}_{SI}) \mathcal{D} \in \mathbb{C}^{NL \times M}$  can be represented as:

$$egin{aligned} \widehat{oldsymbol{\mathcal{G}}} &= \left( \left( \mathbf{X}_{\mathrm{p}}^{\dagger} 
ight)^{\mathrm{T}} \otimes \mathbf{I}_{N} 
ight) \left( \overline{\mathbf{Y}}_{\mathcal{S}} - \left( \mathrm{vec} \left\{ \widehat{\mathbf{H}}_{\mathcal{S}\mathcal{U}} \mathbf{X}_{p} 
ight\} \otimes \mathbf{1}_{1 imes M} 
ight) 
ight) \ &= \left( \mathbf{H}_{\mathcal{I}\mathcal{U}}^{\mathrm{T}} \otimes \mathbf{H}_{\mathcal{S}\mathcal{I}} 
ight) \mathcal{D}_{\Phi} + \left( \left( \mathbf{X}_{\mathrm{p}}^{\dagger} 
ight)^{\mathrm{T}} \otimes \mathbf{I}_{N} 
ight) \left( \overline{\mathbf{W}}_{\mathcal{S}} - \mathrm{vec} \left\{ \widetilde{\mathbf{H}}_{\mathcal{S}\mathcal{U}} \mathbf{X}_{p} 
ight\} \otimes \mathbf{1}_{1 imes M} 
ight) \end{aligned}$$

## **Optimal Active EB Design for a Given PIS Design**

• Assuming perfect CSI availability at S, the joint optimization problem can be formulated as:

 $\mathcal{O}_{\mathbf{J}}: \max_{\mathbf{f}_{\mathbf{A}}, \mathbf{f}_{\mathbf{P}}} \mathcal{P}_{\mathcal{U}}, \qquad \text{subject to (s. t.):} \\ (C1): \|\mathbf{f}_{\mathbf{A}}\|^{2} \leq 1, \qquad (C2): |[\mathbf{f}_{\mathbf{P}}]_{i}| = 1, \forall i \in \mathcal{M}$ 

• For a given PIS design, active EB designing problem is given by:

$$\mathcal{O}_{A}: \max_{\mathbf{f}_{A}} \|\mathbf{G} \mathbf{f}_{A}\|^{2} = \operatorname{Tr}\left\{\mathbf{G} \mathbf{f}_{A} \mathbf{f}_{A}^{H} \mathbf{G}^{H}\right\}, \text{ s. t. (C1)}$$

- The globally-optimal solution for active EB is characterized via the principal eigenvector:  $\begin{bmatrix} \mathbf{f}_A^{\mathrm{op}} \triangleq \mathbf{v}_{\max} \left\{ \mathbf{G}^{\mathrm{H}} \, \mathbf{G} \right\}$
- The maximum value of the objective of active EB problem is **bounded** as:

$$\lambda_{\max}\left\{\mathbf{G}^{H}\mathbf{G}\right\} \leq \left\|\mathbf{H}_{\mathcal{S}\mathcal{U}}\right\|^{2} + \left\|\mathbf{H}_{\mathcal{S}\mathcal{I}}\mathrm{diag}\left\{\mathbf{f}_{P}\right\}\mathbf{H}_{\mathcal{I}\mathcal{U}}\right\|^{2} + 2\operatorname{Re}\left\{\operatorname{Tr}\left\{\mathbf{H}_{\mathcal{S}\mathcal{U}}^{H}\mathbf{H}_{\mathcal{S}\mathcal{I}}\mathrm{diag}\left\{\mathbf{f}_{P}\right\}\mathbf{H}_{\mathcal{I}\mathcal{U}}\right\}\right\}$$

#### PS Design Maximizing Sum Received Power via PIS

• Relaxing the nonconvex constant-envelope constraint (C2) to (C3), optimization problem reduces to:

$$\mathcal{D}_{P1} : \max_{\mathbf{f}_{P}} \quad \|\mathbf{H}_{\mathcal{SI}} \operatorname{diag} \{\mathbf{f}_{P}\} \mathbf{H}_{\mathcal{IU}} \|^{2}$$
  
s. t. (C3) :  $\|\mathbf{f}_{P}\|^{2} \leq M$ .

• The underlying sub-gradient Karush-Kuhn-Tucker (KKT) condition is given by:

$$\frac{\partial \mathcal{L}_{\mathrm{P1}}}{\partial \mathbf{f}_{\mathrm{P}}} = \mathbf{f}_{\mathrm{P}}^{\mathrm{H}} \boldsymbol{\mathcal{D}}^{\mathrm{T}} \left( \mathbf{H}_{\mathcal{I}\mathcal{U}}^{*} \otimes \mathbf{H}_{\mathcal{SI}}^{\mathrm{H}} \right) \left( \mathbf{H}_{\mathcal{I}\mathcal{U}}^{\mathrm{T}} \otimes \mathbf{H}_{\mathcal{SI}} \right) \boldsymbol{\mathcal{D}} - \nu_{\mathrm{P1}} \mathbf{f}_{\mathrm{P}}^{\mathrm{H}} = \mathbf{0}_{1 \times M}$$

- Above can be simplified to the eigenvalue problem form with underlying globally-optimal being the principal eigenvector  $\mathbf{f}_{\mathrm{P}}^{\mathrm{op1}} \triangleq v_{\mathrm{max}} \{ \boldsymbol{\mathcal{G}} \boldsymbol{\mathcal{G}}^{\mathrm{H}} \}$  of matrix  $\boldsymbol{\mathcal{G}} \boldsymbol{\mathcal{G}}^{\mathrm{H}}$
- Now, as the optimal passive EB must satisfy the practical PIS design constraint (C2), the first proposed low-complexity PIS design can be obtained as the minimizer of:

$$\mathcal{O}_{\mathrm{L}}: \min_{\mathbf{f}_{\mathrm{P}}} \|\mathbf{f}_{\mathrm{P}} - \mathbf{f}_{\mathrm{P}}^{\mathrm{op1}}\|^{2}, \quad \text{s. t. (C2)}$$

• The globally-optimal solution of above problem is:

s: 
$$\mathbf{f}_{\mathrm{P}}^{\mathrm{pr1}} \triangleq \exp\left\{j / \mathbf{v}_{\mathrm{max}}\left\{\boldsymbol{\mathcal{G}}\,\boldsymbol{\mathcal{G}}^{\mathrm{H}}\right\}\right\}$$

#### Analytical PIS Design for Constructive Interference

• The second low-complexity PIS design is aimed to ensure that the reflected signals from PIS get coherently added up at the users with ones received directly from S

$$\mathcal{O}_{P2}: \max_{\mathbf{f}_{P}} \operatorname{Tr}\left\{\mathbf{H}_{\mathcal{S}\mathcal{U}}^{H} \mathbf{H}_{\mathcal{S}\mathcal{I}} \operatorname{diag}\left\{\mathbf{f}_{P}\right\} \mathbf{H}_{\mathcal{I}\mathcal{U}}\right\}, \quad s. t. (C3)$$

• The sub gradient KKT condition for the above optimization problem is given by:

$$\frac{\partial \mathcal{L}_{\mathrm{P}_{2}}}{\partial \mathbf{f}_{\mathrm{P}}} = \left(\operatorname{vec}\left\{\mathbf{H}_{\mathcal{S}\mathcal{U}}\right\}\right)^{\mathrm{H}} \left(\!\mathbf{H}_{\mathcal{I}\mathcal{U}}^{\mathrm{T}} \otimes \mathbf{H}_{\mathcal{S}\mathcal{I}}\!\right) \boldsymbol{\mathcal{D}} - \nu_{\mathrm{P}_{2}} \mathbf{f}_{\mathrm{P}}^{\mathrm{H}} \!=\! \mathbf{0}_{1 \times M}$$

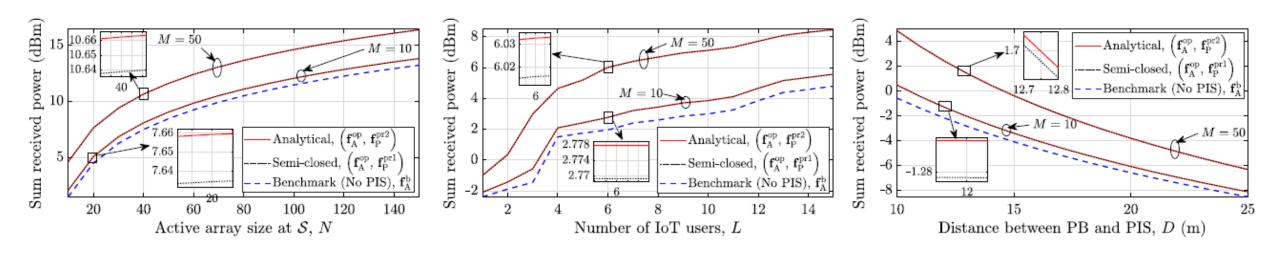
• Solving above in passive EB design leads to globally-optimal solution of the above problem as:

$$\mathbf{f}_{\mathrm{P}}^{\mathrm{op2}} \triangleq \frac{1}{\nu_{\mathrm{P}_{2}}} \, \boldsymbol{\mathcal{G}}^{\mathrm{H}} \operatorname{vec} \left\{ \mathbf{H}_{\mathcal{S}\mathcal{U}} \right\}$$

• Now again here noting that scalar  $v_{P2}$ , the closed-form expression for the 2<sup>nd</sup> optimal constant-envelope PIS design as obtained by solving the underlying LS error minimization problem, can be written as:

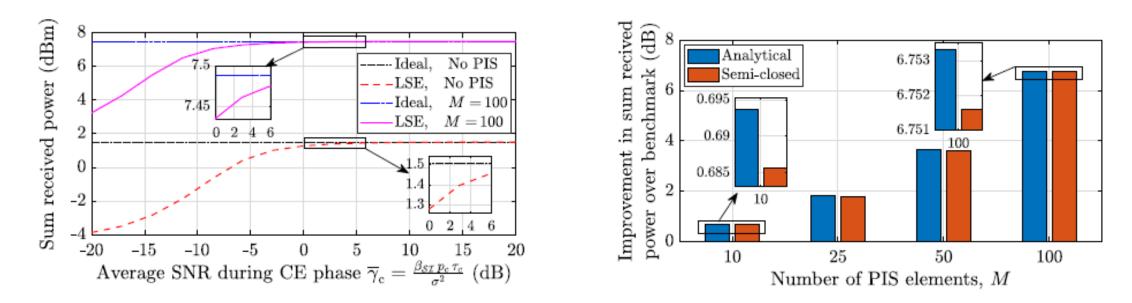
$$\mathbf{f}_{\mathrm{P}}^{\mathrm{pr2}} \triangleq \exp\left\{j / \mathcal{G}^{\mathrm{H}} \operatorname{vec}\left\{\mathbf{H}_{\mathcal{SU}}\right\}\right\}$$

#### Performance Comparison and Impact of Key Parameters



- We compare the performance of the two proposed passive EB designs (semi-closed-form and analytical PIS designs) for different values of key system parameters like active array size N at PB, PIS size M, number L of IoT users, and the distance D between PB & PIS
- The benchmark scheme considered here sets its active EB design assuming no PIS availability
- The average gain as achieved by using M = 50 over M = 10 remains almost constant around 2.6dB for varying N
- 11.7 dB gain is achieved by both schemes when N is increased from 10 to 150
- With increasing L, the sum received power performance improves by 7.65dB and 9.43dB, respectively, for M = 10 and M = 50
- With the field size D increased from 10m to 25m, the performance degrades by 4.5dB and 1.9dB, respectively, for M = 10 and M = 50

#### Impact of CE Errors and Gains



- The quality of the proposed estimators improves with increasing SNR for both with and without PIS settings
- For SNR higher than 5 and 10dB, the proposed estimator approaches the perfect CSI case for M = 0 and M = 100
- Analytical PIS design is better than the semi-closed-form one with a performance gap of < 0.01dB
- Using LS estimators provides an additional improvement of 0.01dB, 0.03dB, 0.06dB, and 0.13dB, for M as 10, 25, 50, and 100
- An improvement of 0.7dB to 6.8dB is achieved by the proposed CE with optimal EB for M = 10 and M = 100

## **Concluding Remarks**

- We introduced an on-off based CE protocol for multiuser PET system
- Derived the closed-form expressions for the underlying LS estimators
- Novel analytical expressions for the jointly-optimal active and passive EB designs
- Demonstrated **significant performance enhancement** over the benchmark
- The developments can be extended for exploring the efficacy of PET in improving information rates and spectral efficiencies in multiuser systems

#### Thank you for your attention!

# For questions and feedback, please contact: d.mishra@unsw.edu.au