

FULL-DUPLEX MULTIFUNCTION TRANSCIEVER WITH JOINT CONSTANT ENVELOPE TRANSMISSION AND WIDEBAND RECEPTION

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Introduction

- FD capable system for simultaneous jamming, radar, data transmission and spectral monitoring.

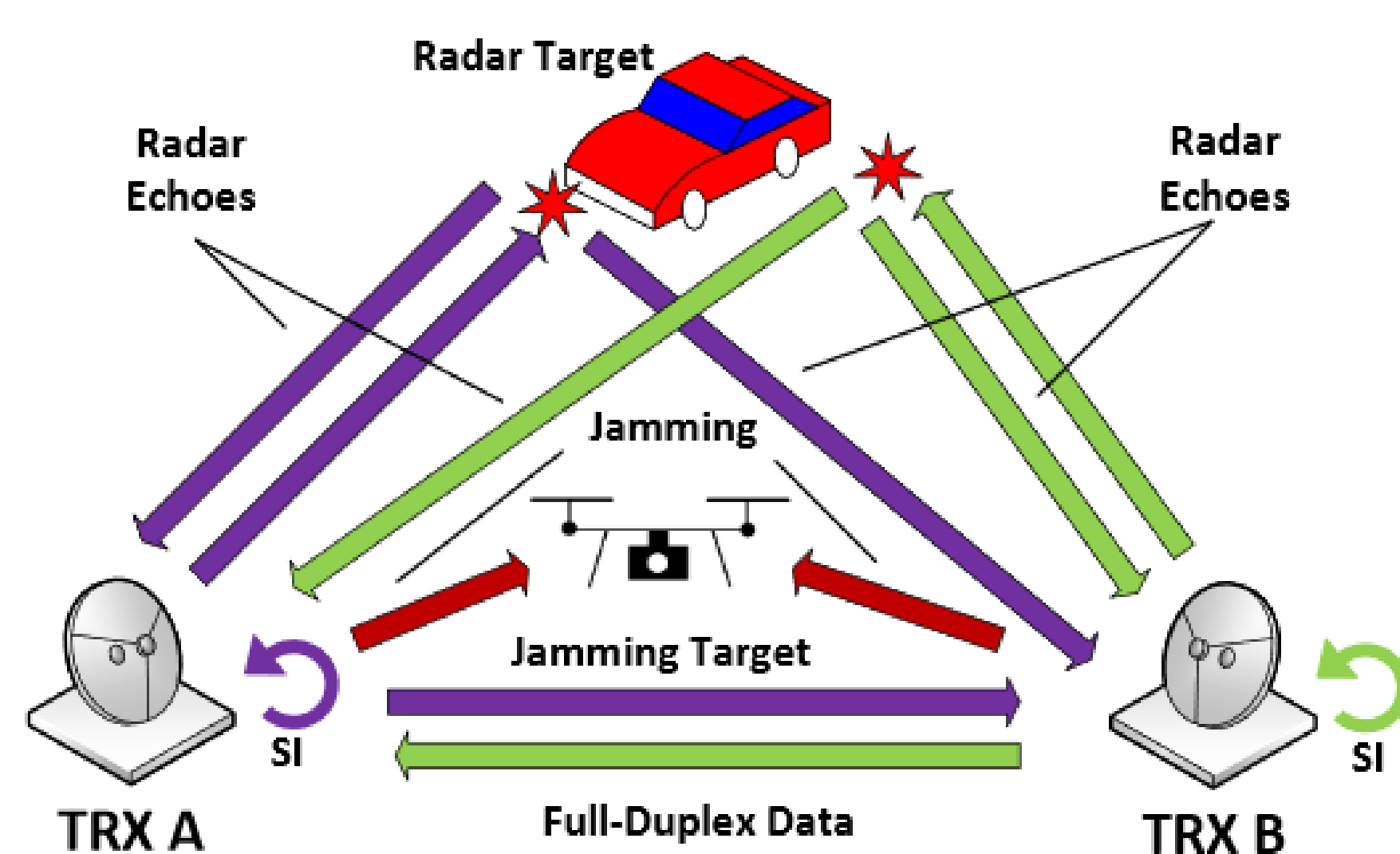
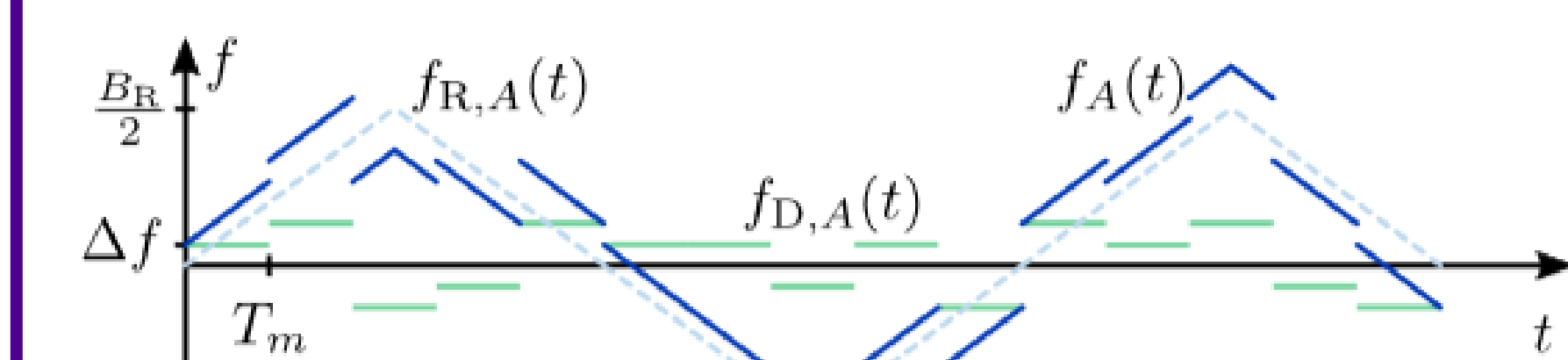
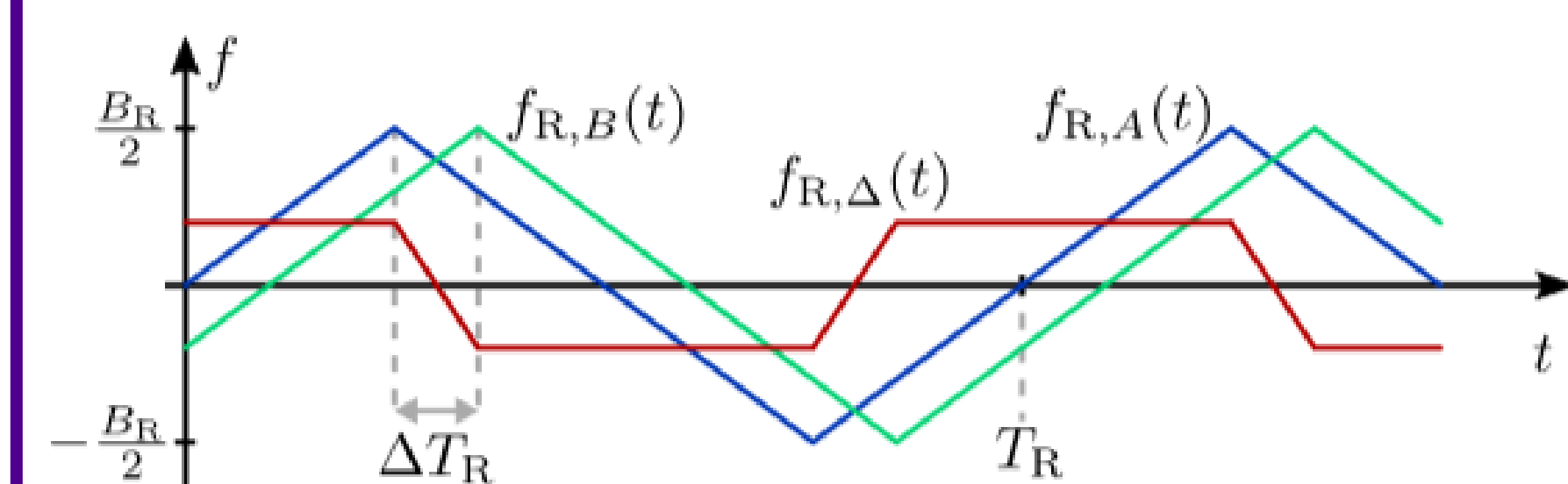


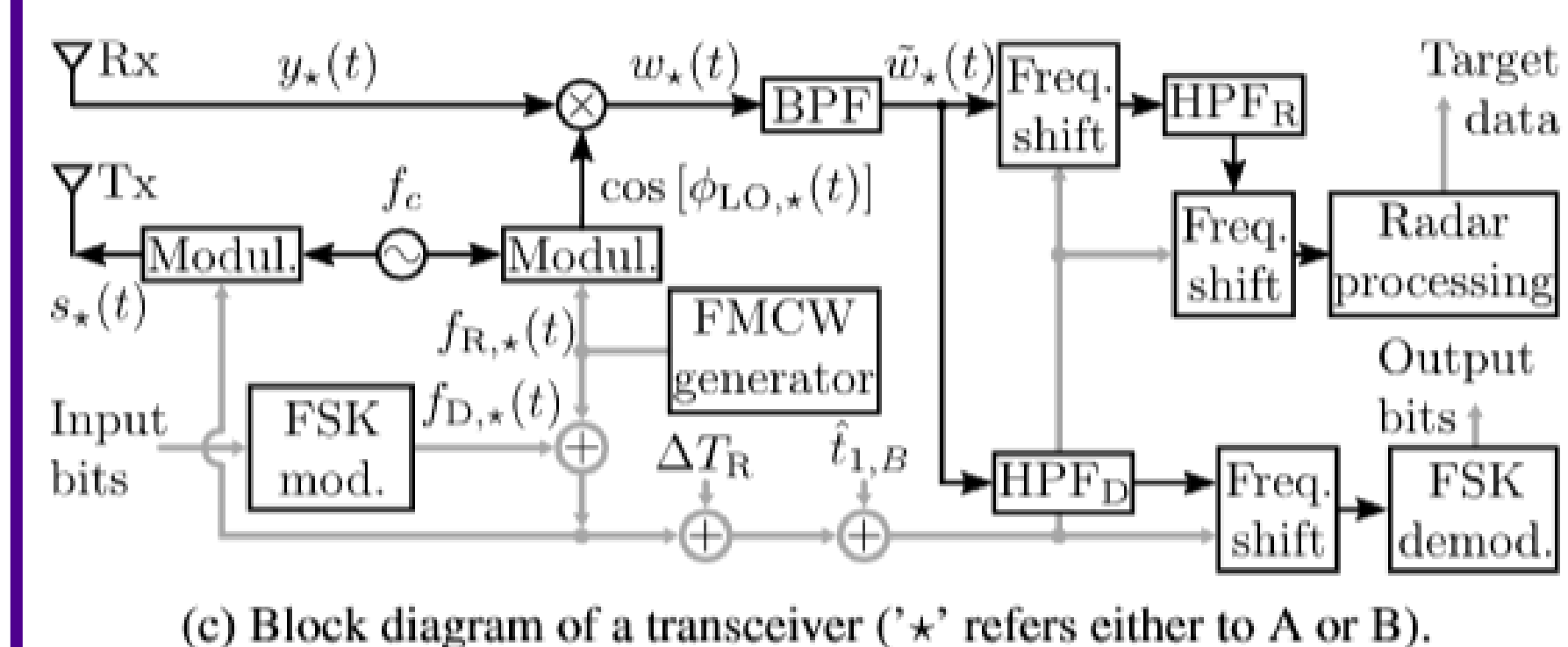
Fig. 1. A concept picture of the novel multifunction system.



(a) Generation of the transmitted waveform $f_A(t)$ at baseband.



(b) Baseband FMCW waveforms of transceivers A and B.



(c) Block diagram of a transceiver ('*' refers either to A or B).

System model

- FMCW triangular sweep radar waveform combined with FSK modulated data (1)-(4).

$$f_{R,*}(t) = \begin{cases} -\frac{B_R}{2} + \frac{\rho t}{m}, & (m-1) < \frac{t-\delta_*}{T_R} \leq \frac{2m-1}{2} \\ +\frac{B_R}{2} - \frac{\rho t}{m}, & \frac{2m-1}{2} < \frac{t-\delta_*}{T_R} \leq m, \end{cases} \quad (1)$$

$$f_{D,*}(t) = \frac{\Delta f}{2} \alpha(t), \quad \alpha(t) \in \{\pm 1, \pm 3, \dots, \pm(2M-1)\} \quad (2)$$

$$\phi_*(t) = 2\pi \left[f_c t + \int_0^t (f_{D,*}(\tau) + f_{R,*}(\tau)) d\tau \right] \quad (3)$$

$$f_*(t) = \frac{1}{2\pi} \phi_*'(t) \quad (4)$$

- At reception, received signal is downconverted with the FMCW signal, with frequencies $f_R(t)$.

- Sweeping signals have fixed carrier frequencies equal to the time difference $t_{*,k}$ of the echo k from TRX \star .
- Due to triangular FMCW waveform, the carrier frequency shifts rapidly between positive and negative carrier during ΔT_R .
- Previously fixed signals are now sweeping the band according to the FMCW signal.

- All of the TRXs need to have the same FMCW bandwidth B_R and sweep rate ρ .

- The fixed delays δ_* are used to offset the sweeping signals to reduce overlap.
 - $\Delta T_R = \delta_B - \delta_A$.

Fig. 2. (a) Example waveforms of the FMCW, FSK and the combined signal. (b) Example waveform of the FMCW signal from TRX B after downconversion at TRX A. (c) Transceiver structure and signal processing.

Multifunction receive processing

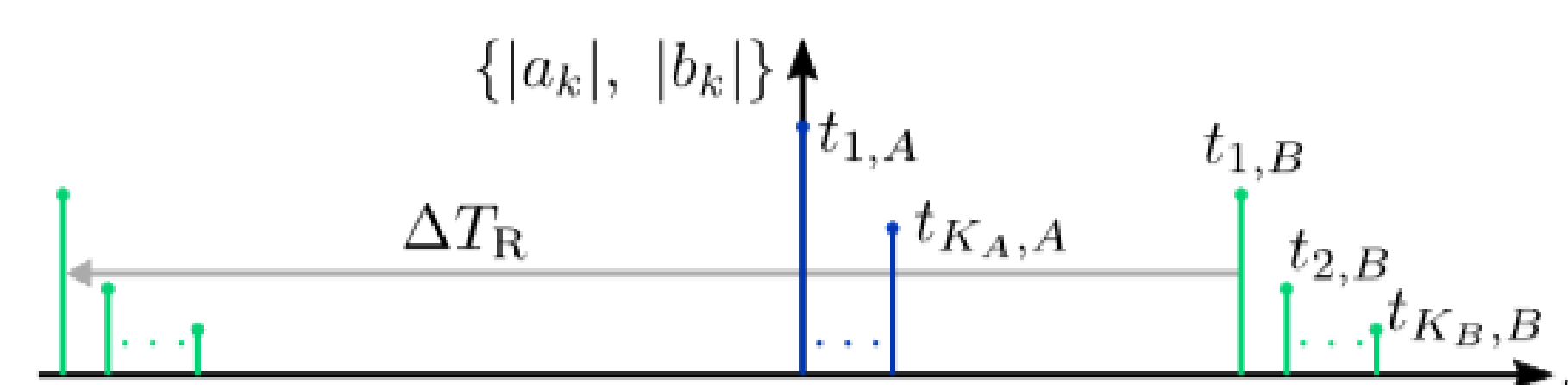


Fig. 3. One-sided spectrum of the downconverted signal, where the shift to the negative frequencies during ΔT_R is shown.

- After downconversion, radar information is in the center frequency of the echoes, data is in the frequency shifts caused by the FSK.
 - Sweep compensation and highpass filters can be used to remove interference.

- For data reception, SI and echoes removed with a HPF with a cutoff frequency of

$$f_{HPFD} = \frac{\Delta f}{2}(2M-1) + \rho t_{K,A} \quad (5)$$

- Sweeping of both TRX compensated with multiplication operations:

$$f_{B,A}(t) = f_B(t - t_{1,B}) - f_{LO,A}(t) = f_{D,B}(t - t_{1,B}) + f_{R,B}(t - t_{1,B}) - f_{R,A}(t) \quad (6)$$

$$\tilde{f}_B(t) = f_{B,A}(t) + (f_{R,A}(t) - f_{R,B}(t - t_{1,B})) = f_{D,B}(t - t_{1,B}) \quad (7)$$

- The FSK data from TRX B can be demodulated through normal means (7).
- Similar compensation and filtering can be done to remove the TRX B signal before radar calculations.

Simulation results

- Two FSK-FMCW transceivers, A and B.
- Following parameters were used in the simulations:
 - FSK-FMCW parameters
 - $M = 1$ and 3 (BPS), $\Delta f = 200$ kHz, symbol duration 0.1 ms.
 - $B_R = 80$ MHz, $\rho = 33 \mu\text{s}$ (4.8 MHz/ μs).
 - $\Delta T_R = 4.2 \mu\text{s}$ (20 MHz) difference between TRX A and B.
 - Single radar target
 - Doppler velocity = 100 m/s.
 - RCS = 200 m²
 - Distances $20, 60$ and 100 m.

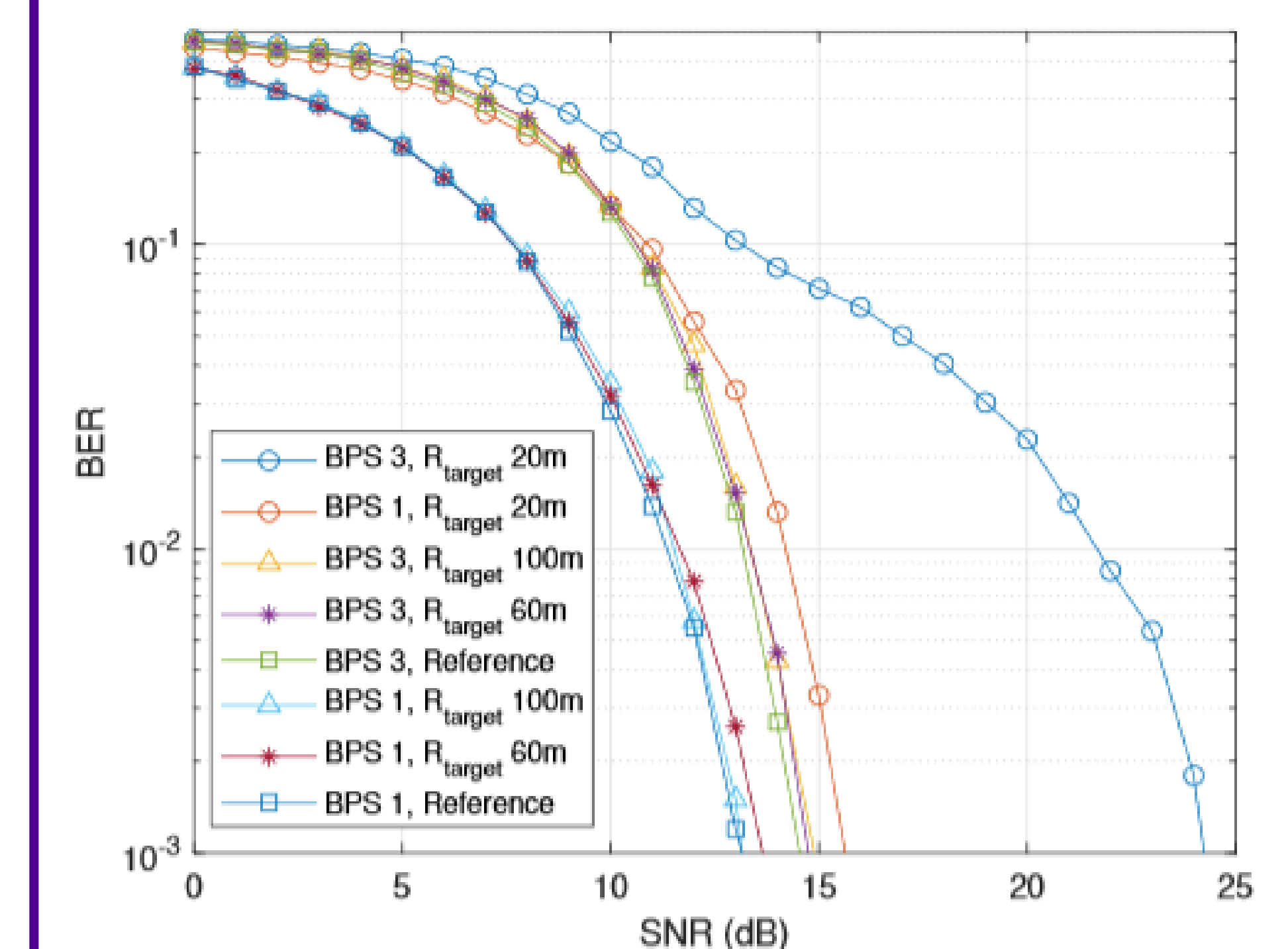


Fig. 4. Simulated FSK demodulation performance. The reference case is half-duplex operation without FMCW sweeping.

- The FSK demodulation works as well as the reference case when the radar target is at least 60 m away.
- Radar performance was found to be as good as the reference case when TRX B signal's SNR was under several tens of decibels.