IEEE ICASSP 2022

Model-Based Reconstruction for Collimated Beam Ultrasound Systems

Abdulrahman (Abdu) Alanazi, Purdue University, ECE Singanallur Venkatakrishnan, Oak Ridge National Lab Hector Santos-Villalobos, Oak Ridge National Lab Gregery T. Buzzard, Purdue University, Math Charles A. Bouman, Purdue University, ECE

Challenges in NDT?

•Some of the major challenges:

- Detecting flaws in multilayered objects that can be accessed from only one side.
- Non-linear effects such reverberations.
- Direct arrival signals.



Collimated-beam systems use carefully crafted acoustic beams with side lobes suppressed and transducer diffraction minimized to provide deep penetration and high spatial resolution

MAP or Regularized Inversion



- Forward model: $f(x) = -\log p(y|x)$
- Prior model: $h(x) = -\log p(x)$
- MAP or regularized inversion: $\hat{x} \leftarrow \arg \min_{x} \{f(x) + h(x)\}$

System Model

Assuming a linear system, we seek to reconstruct an image x using a mathematical model of the form

y = Ax + Dg + w

- *y* is the observed data,
- *A* is the system matrix,
- *D* a matrix whose columns form a basis for the possible direct arrival signals,
- *g* is a scaling coefficient vector for *D*,
- *w* is a Gaussian random vector with distribution $N(0, \sigma^2 I)$.

Transfer Functions

• For the homogeneous medium shown in Fig. 1, the transfer function from point r_i to r_j is

$$G(v, f) = \tau \exp\left\{-(\alpha c |f| + j2\pi f)\left(\frac{\|v - r_i\| + \|r_j - v\|}{c}\right)\right\},\$$

where

- τ is the transmittance coefficient of the front surface of the medium,
- α is the attenuation coefficient in s/m, and
- *c* is the sound speed in m/s in the medium.



Fig.1 homogeneous medium



Fig.2 Multi-layer media

So, the multi-layer media shown in Fig. 2, the transfer function from r_i to r_j

$$G(v,f) = \prod_{l=1}^{L} \tau_l e^{\left(\gamma_l(v)|f| + 2j\pi f T_l(v)\right)}$$

where

- *L* is the total number of layers,
- τ_l is the transmittance coefficient of the front surface of the l^{th} layer,
- $\gamma_l(v) = c_l \alpha_l T_l(v),$
- c_l is the acoustic speed in m/s in the l^{th} layer,
- α_l is the attenuation coefficient in s/m in the l^{th} layer,
- and $T_l(v)$ is the travel time in seconds between the front and back interface of the l^{th} layer.

Time Delay Computation in Multi-layers

• Based on Snell's law, the time delay from r_i to v to r_j is given by

$$T(v) = \sum_{l=1}^{L} \frac{\sqrt{z_{i,l}^2 + \eta_{i,l}^2} + \sqrt{z_{j,l}^2 + \eta_{j,l}^2}}{c_l}$$

where $z_{i,l} = \eta_{i,l} \tan(\theta_{i,l})$ and $z_{j,l} = \eta_{j,l} \tan(\theta_{j,l})$, $l = 1, 2, \dots, L$.

The height of v as a function of $\theta_{i,l}$ is $\sum_{l=1}^{L} z_{i,l} = \eta_{i,1} \tan(\theta_{i,1}) + \dots + \eta_{i,L} \tan(\theta_{i,L})$



• From Snell's law, we know that

$$\theta_{i,k} = \sin^{-1}\left(\sin\left(\theta_{i,k-1}\right)\frac{c_k}{c_{k-1}}\right), \forall k \in \{2, 3, \dots, L\}.$$

The effective time delay is then computed using <u>Binary Search</u> by finding the angle of refraction and solving for the minimum distance.

Received signal & system matrix

• In frequency space, the received signal is proportional to

$$Y(v,f) = -x(v)S(f) \prod_{l=1}^{L} \tau_l e^{-(\gamma_l(v)|f| + 2j\pi f T_l(v))}$$

where x(v) in m^{-3} is the reflection coefficient for the voxel v and S(f) the Fourier transform of the transmitted signal.

• Then the time-domain **received signal** for a reflection from location v is given by

$$y(v,t) = x(v)h(\gamma(v),t-T(v)),$$

where

$$h(\gamma(v),t) = \mathcal{F}^{-1}\left\{-S(f)e^{-\gamma(v)|f|}\right\}$$

and \mathcal{F}^{-1} is the inverse Fourier transform.

• In order to reduce computation, we make the approximation that

$$\tilde{h}(\gamma, t) = h(\gamma, t) \operatorname{rect}\left(\frac{t}{t_0} - \frac{1}{2}\right)$$

where t_0 is a constant based on the assumption that $h(\gamma, t)$ is equal to zero for $t > t_0$.

• The signal received at time t by transducer r_j in response to the transmission from r_i is computed by summing over all voxels v to obtain

$$\tilde{y}_{i,j}(t) = \sum_{v} \tilde{h}(\gamma(v), t - T(v)) x(v)$$

• This linear relationship between x(v) and y(t) determines a single row of the system matrix A in the time domain.

Collimated Beams

• Define a function $\phi_{s,r}(v)$ that has a value ranging from 0 to 1. Then, we modify $\tilde{y}_{i,j}(t)$ to

$$\tilde{y}_{i,j}(t) = \sum_{v} \tilde{h}(\gamma(v), t - T(v)) \phi(v)^{(\beta)} x(v)$$

• The function $\phi_{s,r}(v)$ depends on the incident and reflected angles and given by

$$\phi(v)^{(\beta)} = \cos^{\beta} \left(\sum_{p=1}^{L} \theta_{i,p} \right) \cos^{\beta} \left(\sum_{q=1}^{L} \theta_{j,q} \right)$$



(a) A simulated beam profile, $\phi(v)^{(\beta)}$, with (a) $\beta = 1$ and (b) $\beta = 8$. (c) A real beam profile for a well-collimated source.

Forward Model

• Finally, the discretized version of the forward model will be

$$-\log p(y|x,g) = \frac{1}{2\sigma^2} ||y - Ax - Dg||^2 + \text{constant},$$

where

- $y \in \mathbb{R}^{MK \times 1}$ is the measurement,
- σ^2 is the variance of the measurement,
- $A \in \mathbb{R}^{MK \times N}$ is the system matrix,
- $x \in \mathbb{R}^{N \times 1}$ is the image,
- $D \in \mathbb{R}^{MK \times K}$ is the direct arrival signal matrix,
- $g \in \mathbb{R}^{K \times 1}$ is a vector that scales the columns of *D* independently,
- *M* is the number of measurement samples, and
- *N* is the number of pixels.

Prior Model

• We adopt the q-generalized Gaussian Markov Random Field (qGGMRF) for the prior model. With this design, the prior model is

$$p(x) = \frac{1}{z} \exp\left(-\sum_{\{s,r\}\in C} b_{s,r}\rho(x_s - x_r)\right)$$

where z is a normalizing constant, C is the set of pair-wise cliques, and

$$p(\Delta) = \frac{|\Delta|^p}{p\sigma_{g_{s,r}}^p} \left(\frac{\left| \frac{\Delta}{T\sigma_{g_{s,r}}} \right|^{q-p}}{1 + \left| \frac{\Delta}{T\sigma_{g_{s,r}}} \right|^{q-p}} \right),$$

where
$$\sigma_{g_{s,r}} = \sigma_0 \sqrt{m_s m_r}$$
 and $m_s = 1 + (m-1) * \left(\frac{\text{depth of pixel } s}{\text{maximum depth}}\right)^a$

Hence,

$$-\log p(x) = \sum_{\{s,r\}\in C} b_{s,r} \rho(x_s - x_r) + \text{constant} .$$

Optimization of MAP cost function

• After combining the forward and prior models, the MAP estimate is given by

$$(x,g)_{MAP} = \arg\min_{x \ge 0,g} \left\{ \frac{1}{2\sigma^2} \|y - Ax - Dg\|^2 + \sum_{\{s,r\} \in C} b_{s,r} \rho(x_s - x_r) \right\}$$

ICD Algorithm Using Majorization Technique Initialize $x, e \leftarrow y - Ax$ For k iterations { $g = (D^t D)^{-1} D^t e$ $e \leftarrow e - Dg$ For each pixel $s \in S$ { $\tilde{b}_{s,r} \leftarrow \frac{b_{s,r}\rho'(x_s - x_r)}{2(x_s - x_r)}$ $\begin{aligned} \theta_1 &\leftarrow -e^t \mathbf{A}_{*,s} + \sum_{r \in \partial s} \tilde{b}_{s,r}(x_s - x_r) \\ \theta_2 &\leftarrow \mathbf{A}_{*,s}^t \mathbf{A}_{*,s} + \sum_{r \in \partial s} \tilde{b}_{s,r} \end{aligned}$ $\alpha^* \leftarrow \operatorname{clip}\left\{-\frac{\theta_1}{\theta_2}, [-x_s, \infty)\right\}$ $x_{s} \leftarrow x_{s} + \alpha^{*}$ $e \leftarrow e - A_{*,s}\alpha^{*}$

Experimental Results: System geometry



Experimental Results: Synthetic Data Results

- Synthetic data was ٠ generated using the K-Wave simulator.
- The red and green dashed ٠ lines demonstrate the groove and backwall locations, respectively.







UMBIR



Experimental Results: Real Data Results

SAFT





UMBIR





Conclusion

- We proposed our multi-layer UMBIR algorithm designed for ultrasonic collimated beam systems.
- We showed the derivation of our modified forward model for multilayered structures and collimated ultrasonic-transducers.
- Our results demonstrated that our UMBIR shows clear improvements over SAFT and is effective for real data applications.

Thank You!

References

•[1] Asadollahi, A., & Khazanovich, L. (2019). Analytical reverse time migration with new imaging conditions for one-sided nondestructive evaluation of concrete elements using shear waves. Ultrasonics, 99, 105960.

- [2] <u>https://www.nde-ed.org</u>
- [3] <u>https://www.engineersedge.com/calculators/air-density.htm</u>
- [4] <u>http://www.k-wave.org/forum/topic/air-water-reflection</u>

•[5] <u>https://www.nde-</u> ed.org/EducationResources/CommunityCollege/Ultrasonics/Physics/refractionsnells.htm

- [6] <u>http://www.brl.uiuc.edu/Publications/1987/Anderhub-JDMS-281-1987.pdf</u>
- [7] <u>http://www.k-wave.org/documentation/example_tvsp_transducer_field_patterns.php</u>
- [8] <u>http://www.k-wave.org/forum/topic/p_final-and-p_max_all#post-7041</u>

•[9] Davis, E. S. (2018). Development of a Novel 3D Acoustic Borehole Integrity Monitoring System (No. LA-UR-18-21823). Los Alamos National Lab.(LANL), Los Alamos, NM (United States).

Reconstructions of all views



Recons of the 37 positions. The notch can be seen between position 16 and 25.